Estimating Subgrade Infiltration Rates for Post-Construction Stormwater Management Site Planning

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THE OHIO STATE UNIVERSITY

Stormwater Management Program

Overview of Presentation

Infiltration-based post-construction BMPs
Planning level site suitability evaluation
Estimating infiltration rates for preliminary site planning and conceptual design

Relationship between Infiltration Rate and Hydraulic Conductivity

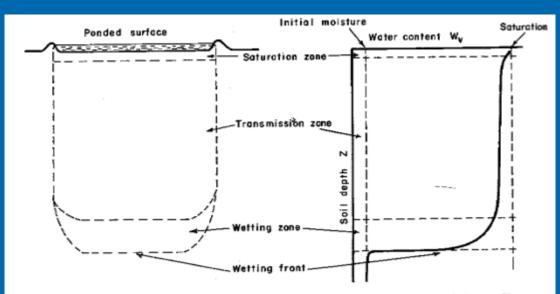


Fig. 12.3. The infiltration moisture profile. At left, a schematic section of the profile; at right, the water content versus depth curve. The common occurrence of a saturation zone as distinct from the transmission zone may result from the structural instability of the surface zone soil. Source: Hillel (1982)

 $i(t) = K_{fs} \frac{\Delta H}{\Delta L} = K_{fs} \frac{H_{pond}(t) + L_f(t) - H_{suction}(t)}{L_f(t)}$

Post-Construction Stormwater Infiltration BMP Options



Bioretention



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Permeable Pavement





Source: Philadelphia Water Department

Underground Infiltration System

Table 4b Infiltration-based Post-Construction Practices

Infiltration Practice	
Bioretention Area/Cell	
Infiltration Basin	
Infiltration Trench	
Permeable Pavement – Infiltration	
Underground Storage – Infiltration	

Source: Ohio EPA. 2018. NPDES Construction Storm Water Permit.

Table 4b Infiltration-based Post-Construction Practices

Infiltration Practice	Maximum Drain Time (t _d) of WQv	
Bioretention Area/Cell	24 hours	
Infiltration Basin	24 hours	
Infiltration Trench		
Permeable Pavement – Infiltration		
Underground Storage – Infiltration		

Source: Ohio EPA. 2018. NPDES Construction Storm Water Permit.

Table 4b Infiltration-based Post-Construction Practices

Infiltration Practice	Maximum Drain Time (t _d) of WQv	
Bioretention Area/Cell	24 hours	
Infiltration Basin	24 hours	
Infiltration Trench	48 hours	
Permeable Pavement – Infiltration	48 hours	
Underground Storage – Infiltration	48 hours	

Source: Ohio EPA. 2018. NPDES Construction Storm Water Permit.

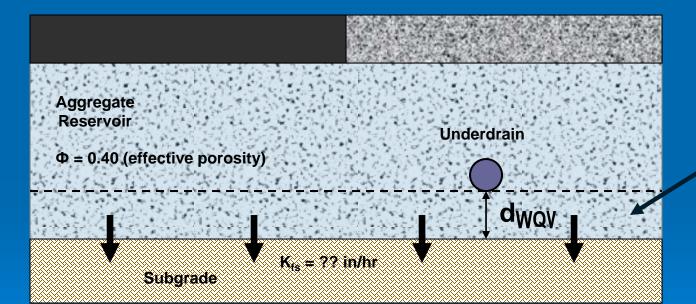
Infiltration Practice	Maximum Drain Time (t _d) of WQv	Minimum Kfs
Bioretention Area/Cell	24 hours	
Infiltration Basin	24 hours	
Infiltration Trench	48 hours	
Permeable Pavement – Infiltration	48 hours	
Underground Storage – Infiltration	48 hours	

Infiltration Practice	Maximum Drain Time (t _d) of WQv	Minimum Kfs
Bioretention Area/Cell	24 hours	No minimum
Infiltration Basin	24 hours	
Infiltration Trench	48 hours	
Permeable Pavement – Infiltration	48 hours	
Underground Storage – Infiltration	48 hours	

Infiltration Practice	Maximum Drain Time (t _d) of WQv	Minimum Kfs
Bioretention Area/Cell	24 hours	No minimum
Infiltration Basin	24 hours	0.5 in/hr
Infiltration Trench	48 hours	0.5 in/hr
Permeable Pavement – Infiltration	48 hours	
Underground Storage – Infiltration	48 hours	

Infiltration Practice	Maximum Drain Time (t _d) of WQv	Minimum Kfs
Bioretention Area/Cell	24 hours	No minimum
Infiltration Basin	24 hours	0.5 in/hr
Infiltration Trench	48 hours	0.5 in/hr
Permeable Pavement – Infiltration	48 hours	$> d_{WQv}/t_d$
Underground Storage – Infiltration	48 hours	$> d_{WQv}/t_d$

WQv Depth for Permeable Pavement and Underground Infiltration Systems

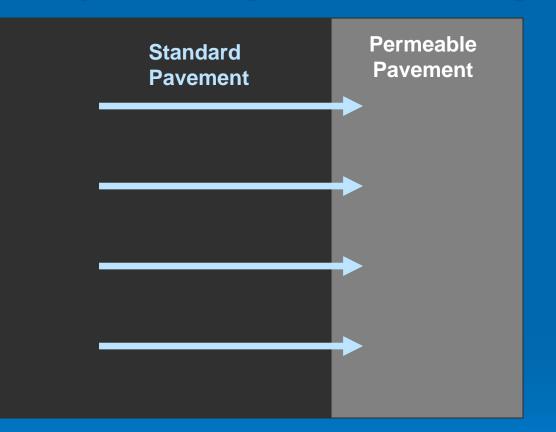


Pavement

Internal Water Storage (IWS) Zone

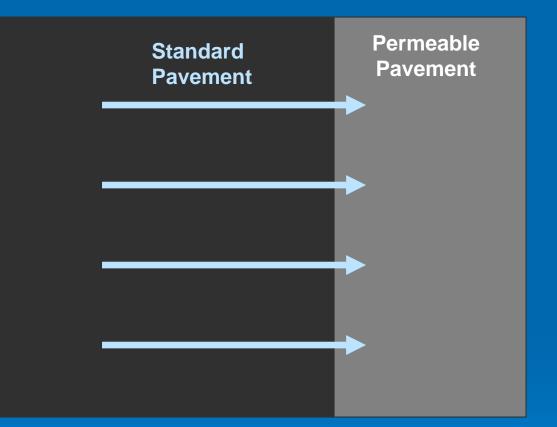


Hydrologic Loading Ratio and Minimum Kfs



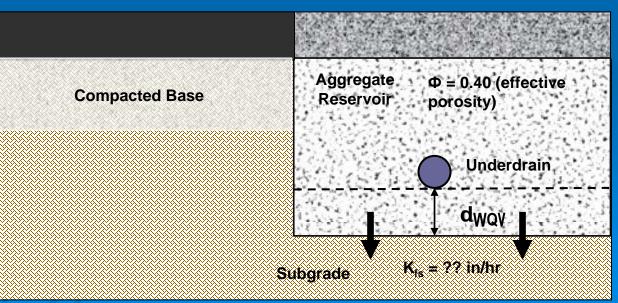
A_{impervious} < 2*A_{permeable} HLR = A_{impervious}/A_{infiltration} = 3.0 $d_{WQv} = WQv/A_{infiltration} = 2.6$ in

Hydrologic Loading Ratio and Minimum Kfs

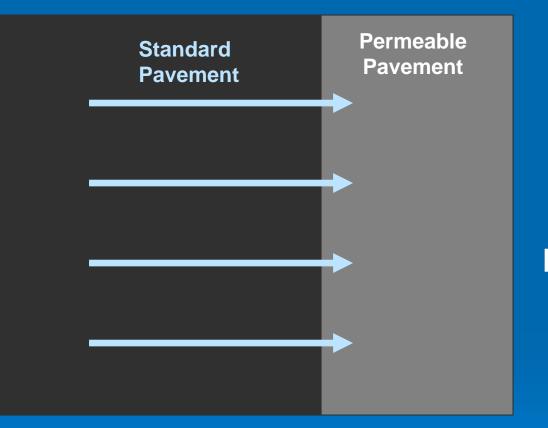


A_{impervious} < 2*A_{permeable} HLR = A_{impervious}/A_{infiltration} = 3.0 $d_{WQv} = WQv/A_{infiltration} = 2.6$ in

Adjusted for aggregate porosity of 0.40 $d_{WQv} = 2.6$ in/0.4 = 6.4 in



Hydrologic Loading Rate and Minimum Kfs



A_{impervious} < 2*A_{permeable} HLR = A_{impervious}/A_{infiltration} = 3.0 $d_{WQv} = WQv/A_{infiltration} = 2.6$ in

Minimum infiltration rate

Kfs(min) = d_{WQv}/t_d = 2.6 in/48 hr = <u>0.054 in/hr</u>

Hydrologic Loading Ratio and Minimum Kfs (subsurface infiltration reservoir, t_d = 48 hr)

A _{infiltration}	A _{impervious}	HLR WQv		dWQv	Kfs(min)	
(acre)	(acre)		(ft3)	<u>(in)</u>	(in/hr)	
1.0	1.0	1	3104	0.9	0.02	
1.0	2.0	2	6207	1.7	0.04	HSG-C
1.0	3.0	3	9311	2.6	0.05	
1.0	5.0	5	15518	4.3	0.09	HSG-B
1.0	10.0	10	31037	8.6	0.18	
1.0	20.0	20	62073	17.1	0.36	HSG-A

WQv Calculator

Water Quality Volume BMP Compliance Worksheets (v3.1 2018-10-23)

Worksheet Contents

D

1 Introduction

- 2 Project Details and WQv Calculation
- 3 Wet Extended Detention Basin
- 4 Wetland Extended Detention Basin (Constructed Wetland)
- 6 Infiltration Basin
- 7 Bioretention
- 8 Infiltration Trench
- 9 Permeable Pavement Infiltration
- 10 Ferneuble Fuvement Extended Detention [Under Deve
- 11 Sand or Media Filter [Under Development]

Step 2 - Trench Bottom Area/Dimensions					
Area that can drain in 48 hr =		ft ²			
5% of A _{imp} =	0	ft ²			
Minimum Infiltration Trench (Bottom) Area =	0	ft ²			
Infiltration Trench (Bottom) Area =		ft			
Trench Width, W _{trench} =		ft			
Trench Length, L _{trench} =		ft ²			
Trench Area/Impervious Area, A _{trench} /A _{imp} =					
Length to Width Ratio (L:W) =		ft/ft			
					_
			 		_
Step 3 - Trench Layer Depths					_
					-
Depth of WQv, d _{WQv} =		ft			_
Aggregate Adjusted WQv Depth, d _{aggr-WQv} =		ft			_
WQv Drawdown Time, t _{WQv} =		hr			_
		-			-
Depth of Surface Gravel Filter Layer, d _{gravel filter} =					_
Depth of Aggregate Storage Layer, d _{storage} =		ft			
Depth of Bottom Sand Filter Layer, d _{sand} =		ft			
Total Depth of Aggregate, d _{aggregate} =	1.17	ft			

WQv Compliance Spreadsheet

- Available for download at Ohio EPA's Storm Water Program website:
- Search "Ohio EPA Storm Water"
- Click "Construction Activities" tab
- Click "Technical Assistance & Permit Compliance Materials"

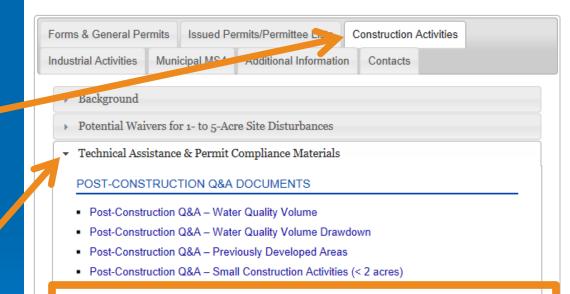
Storm Water Program

Storm water discharges are generated by runoff from land and impervious areas such as paved streets, parking lots, and building rooftops during rainfall and snow events. Storm water often contains pollutants in quantities that could adversely affect water quality. Most storm water discharges are considered point sources and require coverage by a National Pollutant Discharge Elimination System (NPDES) permit. The primary method to control storm water discharges is through the use of best management practices (BMPs).

For information about storm water management at home, visit the Public Interest Center's website.

NEW! Final General Permit for Storm Water Associated with Construction from Oil and Gas Linear Transmission Line and Gathering Line Installation (OHCG00001)

NEW! Final General NPDES Permit for Storm Water Associated with Construction Activity (OHC000005)



POST-CONSTRUCTION SPREADSHEETS

- WQv Compliance Spreadsheet
- Runoff Reduction Spreadsheet

CHECKLISTS

- Storm Water Pollution Prevention Plan (SWP3) Check List
- Construction Site Inspection Checklist



Appropriate Use for Estimates

Methods are available to provide rough estimates of infiltration (exfiltration) rates expected from BMPs such as bioretention or pervious pavement systems.

These methods are appropriate for **preliminary site planning**, i.e., to determine if an LID approach makes sense for a particular site or to develop a ballpark area allocated for infiltration BMPs.

Appropriate Use for Estimates

If moving forward with a design that incorporates infiltration BMPs (i.e., if credit is being taken toward meeting WQv, runoff volume reduction or peak discharge requirements) field measured infiltration tests are necessary to determine a more accurate infiltration rate for sizing and design of BMPs.

Estimating Infiltration Rates for BMPs for Site Planning

- Estimate the depth of excavation for the proposed infiltration BMP
- Identify the soil texture at the proposed depth of excavation
- Estimate infiltration rate by soil texture

Estimate Depth of Excavation for the Proposed Infiltration BMP

Infiltration Practice	Typical Excavation Depth Range
Bioretention Area/Cell	60" – 84" (72")
Infiltration Basin	48" – 72" (60")
Infiltration Trench	48" – 60" (48")
Permeable Pavement – Infiltration	18" – 30" (30")
Permeable Pavement – Infiltration w/Q _{peak}	36" – 96" (60")
Underground Storage – Infiltration	48" – 96" (96")

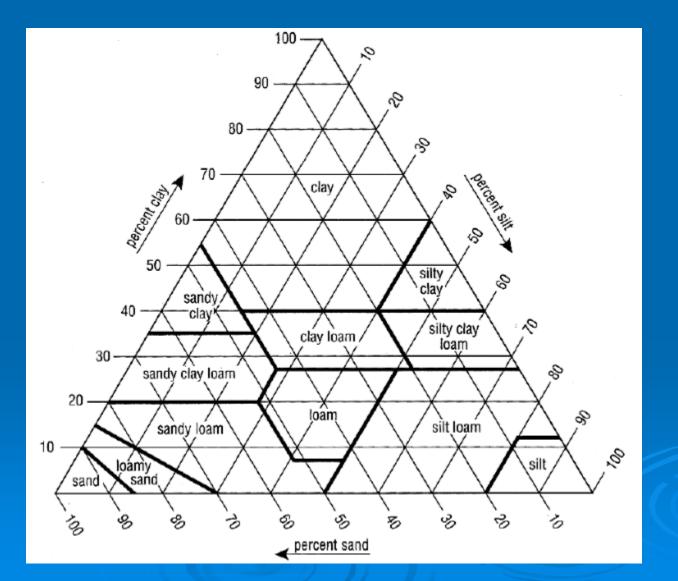
Identify the soil texture at the proposed depth of excavation

In order of preference:

1. Particle or grain size distribution test on soil samples collected at the proposed location and depth (need at least percent sand, silt, and clay).

L												
	Specimen Identi	fication	D100	D60	D30	D10		%Gravel	%Sand	%Silt	%Clay	
	B-2	4.3	19	5.186	0.741	0.063		41.9	47.1	10.5	0.5	
Þ	B-3	1.8	4.75	0.041	0.012	0.002		0.0	15.2	75.3	9.5	
L												
F												
F												
F	Intertek Professional Service Industries, Inc.				GRA	١N	I SIZE I	DISTRIE	BUTION	J		
L		4960 Vulo	can Ave, Suite (•	Project:	MVNU	Сс	ompetition	Field			
L	Columbus, OH 43228			PSI Job No.: 01021470								
	Telephone: (614) 876-8000		00	Location: Mt. Vernon								
	Fax: (614) 876-0548			Ohio								

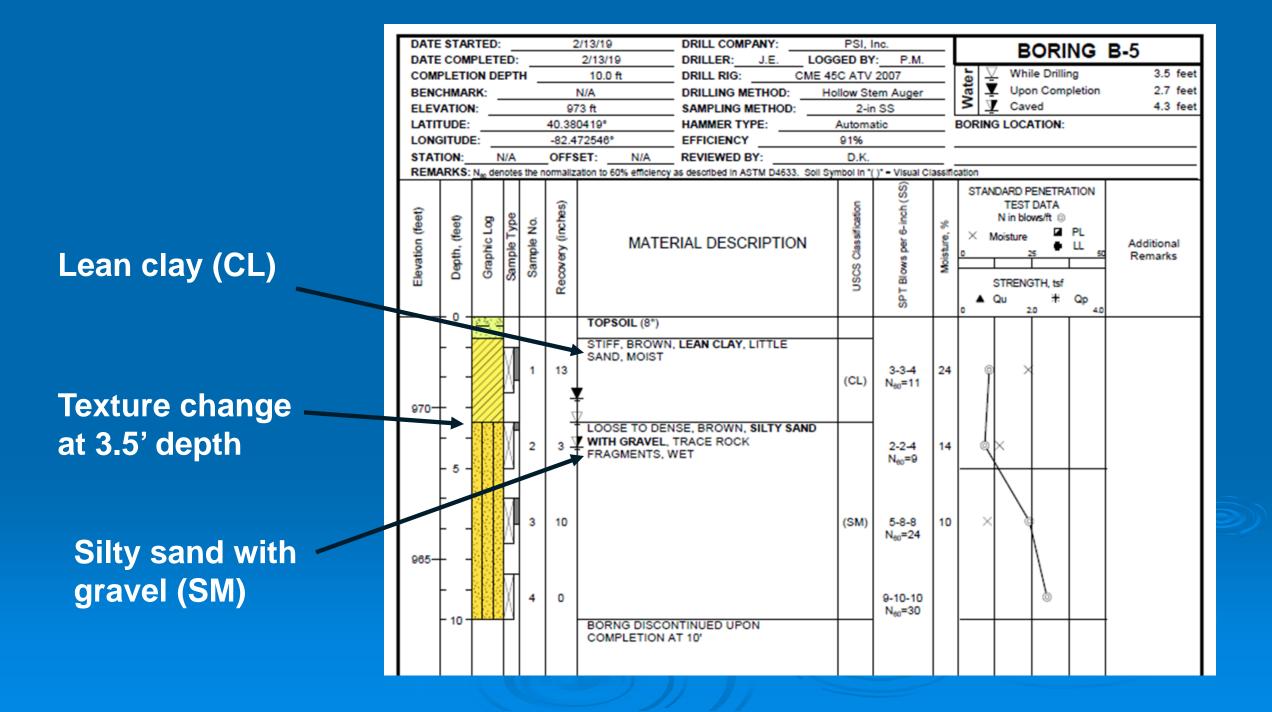
USDA Soil Texture



Identify the soil texture at the proposed depth of excavation

In order of preference:

- 1. Particle or grain size distribution test on soil samples collected at the proposed location and depth (need at least percent sand, silt, and clay).
- 2. Field-conducted soil classification by a certified professional (soil pedologist or geotech).



Translating USCS Classification to USDA Soil Texture

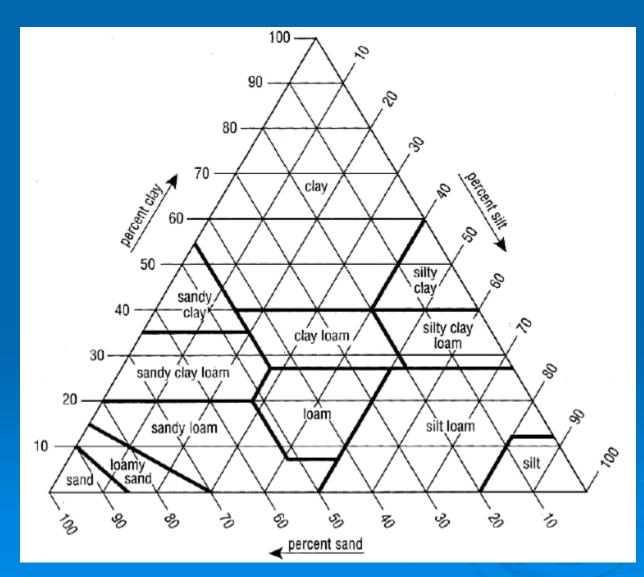
Figure 5. USCS classifications (Ayers et al. 2011) mapped onto the USDA triangle.



Table 13. USCS classification best fit for USDA classification based on Ayers et al. (2011).

	USCS Classification					
USDA Classification	Most Probable	Possible				
Sand	SW, SP	-				
Loamy Sand	SM	SC				
Sandy Loam	SM	-				
Sandy Clay Loam	SC	-				
Sandy Clay	SC	CL				
Loam	ML	-				
Silt Loam	ML	-				
Silt	ML	-				
Clay Loam	CL, MH	_				
Silty Clay Loam	MH	-				
Clay	СН	CL				
Silty Clay	CL, MH	-				
Peat	-	_				

USDA Soil Texture



Field Description

09-24-13

Soil description for the under-construction sediment control basin at Holden Arboretum, Lake County, Ohio. The basin is south/southeast of the visitor's center. The exposed basin wall at the south end of the structure (latitude N 41° 36' 39.7'' and longitude W 81° 18' 03.5'') was described on September 11, 2013.

The area is mapped to Platea silt loam, 2 to 6 percent slopes in Web Soil Survey.

Soil description

Ap1 horizon: 0 to 2 inches; dark grayish brown silt loam, 11% clay, 10% sand; many fine and very fine roots; weak fine and medium granular structure; <1% rock fragments

Ap2 horizon: 2 to 8 inches; dark grayish brown silt loam, 11% clay, 10% sand; very few very fine roots; massive structure do to compaction; <1% rock fragments

Bw horizon: 8 to 26 inches; yellowish brown silt loam, 12% clay, 10% sand, with redoximorphic concentrations (10YR 5/6) and depletions (10YR 6/1); no roots; massive structure do to compaction; <1% rock fragments

Bt horizon; 26 to 39 inches; dark yellowish brown silty clay loam, 32% clay, 8% sand with redoximorphic concentrations (10YR 5/6) and depletions (10YR 6/1); moderate medium and coarse subangular blocky structure; 1% to 2% rock fragments

Btx horizon: 39 to 50 inches (to the bottom of the excavation); dark yellowish brown silt loam, 18% clay, 15% sand with redoximorphic concentrations (10YR 2/1); weak very coarse prismatic structure parting to moderate thin platy structure; 3% to 5% rock fragments; note: this horizon is a fragipan

Steve Prebonick

Soil Scientist, ODNR

Identify the soil texture at the proposed depth of excavation

In order of preference:

- 1. Particle or grain size distribution test on soil samples collected at the proposed location and depth (need at least percent sand, silt, and clay).
- 2. Field-conducted soil classification by a certified professional (soil pedologist or geotech).
- 3. Soil survey texture for appropriate depth based on soil type (soil map unit) at location of proposed practice.

NRCS Web Soil Survey



https://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm

NRCS Web Soil Survey – Soil Map

Search			
Map Unit	Legend		
			G
Knox C	Knox County, Ohio ounty, Ohio (OH08)
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
0284848.00045	Crane silt loam, 1 to 4 percent slopes	6.9	7.2%
	Fox gravelly loam, 0 to 2 percent slopes	7.4	7.7%
	Fox gravelly loam, 2 to 6 percent slopes	41.1	42.9%
66999296	Fox gravelly loam, 12 to 25 percent slopes	4.3	4.5%
	Lobdell silt loam, 0 to 3 percent slopes, occasionally flooded	17.4	18.2%
10 - 40 - 0 - 0 - 40 - 1	Ockley silt loam, Southern Ohio Till Plain, 0 to 2 percent slopes	0.1	0.1%
OcB	Ockley silt loam	95	9.9%

NRCS Web Soil Survey – HSG Map

В

В

B/D

Map unit symbol

Pits, gravel

Ockley silt loam, Southern Ohio Till Plain, 0 to 2 percent slopes

Ockley silt loam, Southern Ohio Till Plain, 2 to 6 percent slopes

Shoals silt loam, 0 to 2 percent slopes, occasionally flooded

CzA

FoA

FoB

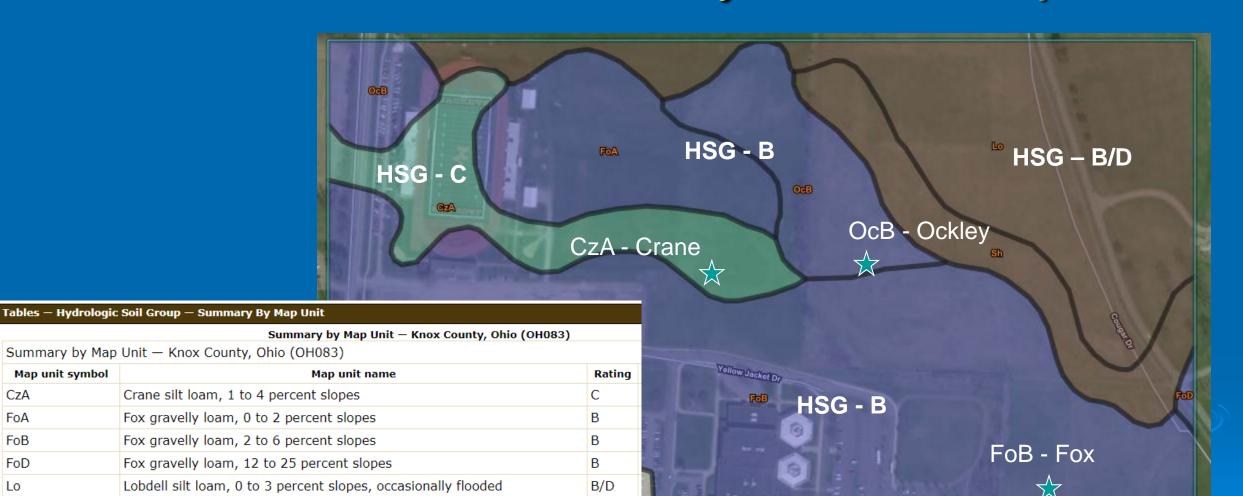
FoD

Lo

OcA

OcB Pg

Sh



NRCS Web Soil Survey – Typical Profile

CzA-Crane silt loam, 1 to 4 percent slopes

Map Unit Setting

National map unit symbol: nlgt Elevation: 600 to 1,000 feet Mean annual precipitation: 30 to 40 inches Mean annual air temperature: 48 to 55 degrees F Frost-free period: 145 to 180 days Farmland classification: Prime farmland if drained

Map Unit Composition

Crane and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of

Description of Crane

Setting

Landform: Outwash plains, terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread Microfeatures of landform position: Mounds Down-clope shape: Linear Actoss-slope shape: Linear Parent material: Loamy glaciofluvial deposits derived from mixed of

Typical profile

- H1 0 to 14 inches: silt loam H2 - 14 to 24 inches: silty clay loam H3 - 24 to 34 inches: clay loam H4 - 34 to 52 inches: gravelly loam
- H5 52 to 60 inches: gravelly loamy sand

Properties and qualities

Slope: 1 to 4 percent Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained Runoff class: Low Capacity of the most limiting layer to transmit water (Ksat): Moder Depth to water table: About 12 to 36 inches Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 25 percent Available water storage in profile: High (about 9.7 inches)

				N	
10	10	24	22	lin'	

Typical profile

- H1 0 to 14 inches: silt loam
- H2 14 to 24 inches: silty clay loam
- H3 24 to 34 inches: clay loam
- H4 34 to 52 inches: gravelly loam
- H5 52 to 60 inches: gravelly loamy sand

Properties and qualities

Slope: 1 to 4 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained Runoff class: Low Capacity of the most limiting layer to transmit wate Depth to water table: About 12 to 36 inches Frequency of flooding: None Frequency of ponding: None

Turning Soil Texture into Kfs

Soil Water Characteristic Estimates by Texture and Organic Matter for Hydrologic Solutions

K. E. Saxton and W. J. Rawls

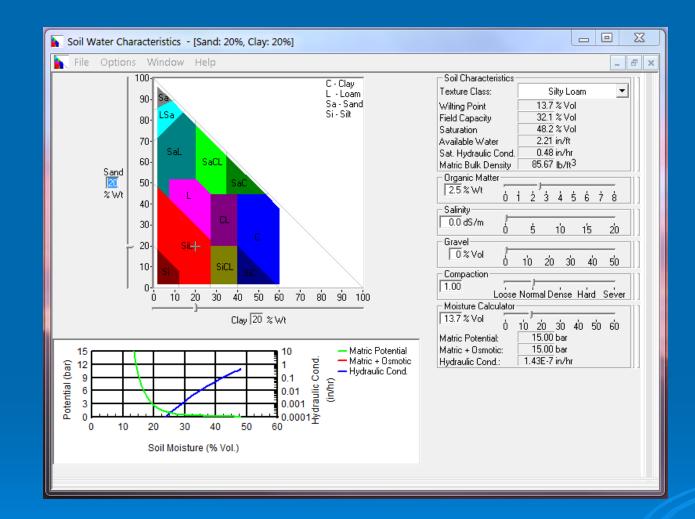
ABSTRACT

Hydrologic analyses often involve the evaluation of soil water infiltration, conductivity, storage, and plant-water relationships. To define the hydrologic soil water effects requires estimating soil water characteristics for water potential and hydraulic conductivity using soil variables such as texture, organic matter (OM), and structure. Field or laboratory measurements are difficult, costly, and often impractical for many hydrologic analyses. Statistical correlations between soil texture, soil water potential, and hydraulic conductivity can provide estimates sufficiently accurate for many analyses and decisions. This study developed new soil water characteristic equations from the currently available USDA soil database using only the readily available variables of soil texture and OM. These equations are similar to those previously reported by Saxton et al. but include more variables and application range. They were combined with previously reported relationships for tensions and conductivities and the effects of density, gravel, and salinity to form a comprehensive predictive system of soil water characteristics for agricultural water management and hydrologic analyses. Verification was performed using independent data sets for a wide range of soil textures. The predictive system was programmed for a graphical computerized model to provide easy application and rapid solutions and is available at http://hydrolab.arsusda. gov/soilwater/Index.htm.

characteristics (Van Genuchten and Leij, 1992). Application of this knowledge is imperative for hydrologic simulation within natural landscapes. However, hydrologists often do not have the capability or time to perform field or laboratory determinations. Estimated values can be determined from local soil maps and published water retention and saturated conductivity estimates, but these methods often do not provide sufficient range or accuracy for computerized hydrologic analyses.

The texture based method reported by Saxton et al. (1986), largely based on the data set and analyses of Rawls et al. (1982), has been successfully applied to a wide variety of analyses, particularly those of agricultural hydrology and water management, for example, SPAW model (Saxton and Willey, 1999, 2004, 2006). Other methods have provided similar results but with limited versatility (Williams et al., 1992; Rawls et al., 1992; Stolte et al., 1994). Recent results of pedotransfer functions (Pachepsky and Rawls, 2005) are an example of modern equations that cannot be readily applied because the input requirements are beyond that cus-

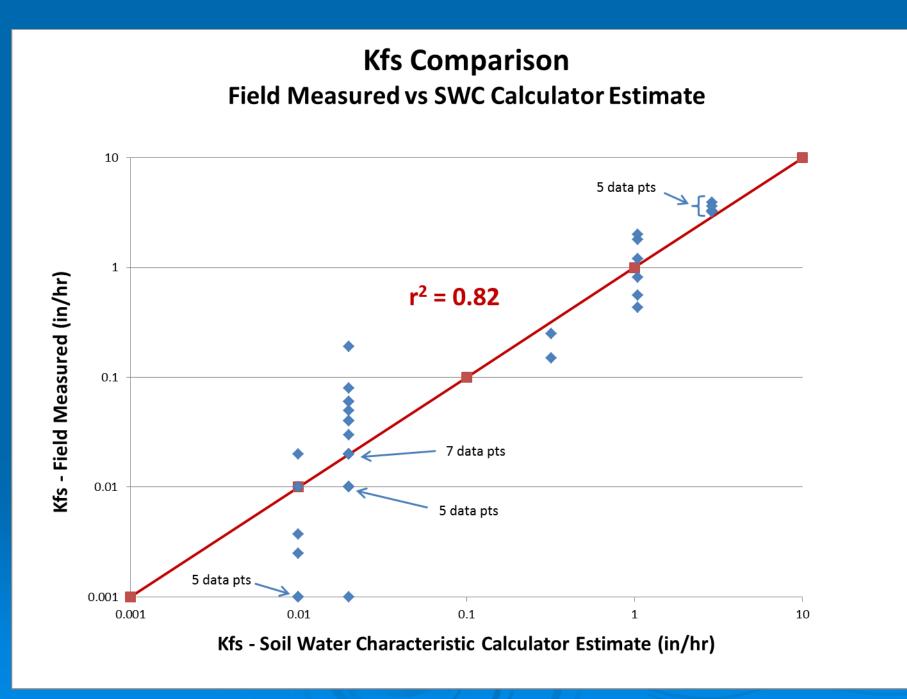
Soil Water Characteristics Calculator



http://hydrolab.arsusda.gov/soilwater/Index.htm

Estimated Infiltration Rates for BMPs for Site Planning

- > Using USDA-ARS Soil Water Characteristic Calculator
 - Select soil texture based on tested particle size distribution or soil survey texture for subgrade layer
 - Reduce organic matter content to 0.05%
 - Increase soil density ("compaction") to "dense" (1.10)



Subgrade K_{fs} Estimates

Subgrade USDA Soil Texture	Clay Content %	Ksat (in/hr)
Sand	< 8	2.8
Loamy Sand	< 15	2.0
Sandy Loam	< 20	0.80
Loam	< 20	0.25
Silt Loam	< 20	0.10
Loam	20 – 27	0.06
Silt Loam	20 - 27	0.03
Silt	< 12	0.05
Sandy Clay Loam	20 – 35	0.07
Clay Loam	27 – 40	0.02
Silty Clay Loam	27 – 40	0.02
Silty Clay	40 – 50	0.01
Sandy Clay	35 – 55	<0.005
Clay	> 40	<0.005

Subgrade K_{fs} Estimates

with Generalized Hydrologic Soil Group

Subgrade USDA	Soil Texture	Clay Content %	Ksat (in/hr)	
Sand		< 8	2.8	
Loamy Sand	HSG-A	< 15	2.0	
Sandy Loam		< 20	0.80	
Loam		< 20	0.25	
Silt Loam	HSG-B	< 20	0.10	
Loam		20 – 27	0.06	
Silt Loam	HSG-C	20 - 27	0.03	
Silt		< 12	0.05	
Sandy Clay Loam		20 – 35	0.07	
Clay Loam	HSG-C or D	27 – 40	0.02	
Silty Clay Loam		27 – 40	0.02	
Silty Clay		40 – 50	0.01	
Sandy Clay	HSG-D	35 – 55	<0.005	
Clay		> 40	<0.005	

Summary

Infiltration BMPs

- Bioretention applicable on most sites
- Infiltration basins and trenches need Kfs \geq 0.5 in/hr
- Permeable pavement and underground infiltration systems good potential for HSG-A, B, C soils

A _{infiltration}	A _{impervious}	HLR	WQv	dWQv	Kfs(min)
(acre)	(acre)		(ft3)	(in)	(in/hr)
1.0	1.0	1	3104	0.9	0.02
1.0	2.0	2	6207	1.7	0.04
1.0	3.0	3	9311	2.6	0.05
1.0	5.0	5	15518	4.3	0.09
1.0	10.0	10	31037	8.6	0.18
1.0	20.0	20	62073	17.1	0.36

Kfs(min) = d_{WQv}/t_d

Summary

Planning level infiltration rate estimates help explore postconstruction BMP options

- Requires identification of soil texture at location and depth of proposed infiltration practice
- Infiltration rate estimates are not sufficient for postconstruction BMP design – representative field measurements of infiltration rate necessary for design

RAINWATER AND LAND DEVELOPMENT PROVISIONAL APPENDIX A-# INFILTRATION ESTIMATES FOR STORMWATER PRACTICE PLANNING DATE: 12/20/18

https://epa.ohio.gov/Portals/35/storm/technical_assistance/ProPractices.pdf

Questions:

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THE OHIO STATE UNIVERSITY

Stormwater Management Program